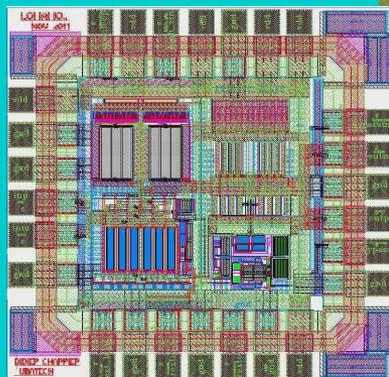


# *“ New developments around the butterfly antenna ”*

**ARENA 2014**  
**June 9-12**  
**Annapolis, USA**



**Didier Charrier**  
  
**Nantes, France**

- **Butterfly Antenna presented 4 years ago**
  - ARENA 2010, Nantes
  - Proceeding: 'Antenna development for astroparticle and radioastronomy experiments', D. Charrier, Nucl. Instr. and Meth. A (2010), doi:10.1016/j.nima.2010.10.141
- **Since that time ...**
  - Antenna radiating elements are electrically the same (bow tie type antenna)
  - development of more accurate models
  - development of a new LNA (LONAMOS) to improve the Butterfly characteristics
  - ...

# Butterfly historic

## ■ October 2008: birth of the Butterfly antenna, original version (6)

- Single polarisation
- Antenna radiator made of electric wire and plastic tube frame
- Use the 'CODALAMP' LNA designed in 2004 at Subatech
- two antennas were installed in the CODALEMA acquisition

## ■ 2009: first upgrade of the Butterfly

- dual polarization antenna
- Antenna radiator element made of rigid aluminium rod
- ---> equip CODALEMA extension

## ■ November 2011: birth of the 'LONAMOS' LNA (3)

- Analog CMOS ASIC designed at Subatech
- better characteristics than CODALAMP LNA
- Production of ~800 circuits

## ■ 2011-2012: second upgrade of the Butterfly (2)

- Design of a mechanic upgrade(wind stabilization) by RWTH Aachen University, III. Physikalisches Institut A, Aachen
- ---> equip AERA II and III

## ■ 2013 : third upgrade of the Butterfly

- CODALAMP is replaced by LONAMOS
- The LNA of the 60 antenna of CODALEMA are substituted

*Butterfly, original version*



*Butterfly, upgrade 1*



*Butterfly, upgrade 2*



# The Butterfly is an active antenna

	Antenna radiating element	LNA	Target
Bandwith	X	X	↗
$\Delta$ Group delay	X	X	↘
Sensitivity	X	X	↗
Linearity		X	↗
Isotropy	X		↗

**==> the LNA is as important as the Antenna radiating element for the overall active antenna characteristics**

# The Butterfly radiating element



- **The butterfly radiating element is a bow-tie dipole**
  - Trade off between a low Q factor - low group delay variation and mechanical complexity
- **The half perimeter length is ~1.6 m**
  - resonance frequency around 45MHz to maximize S/N in [20-80]MHz
- **The height is ~1.5m**
  - Trade off between low frequency antenna efficiency and high frequency isotropy

- **Noise sources**

- LNA noise
- Antenna losses
- Galactic noise temperature

- **Signal**

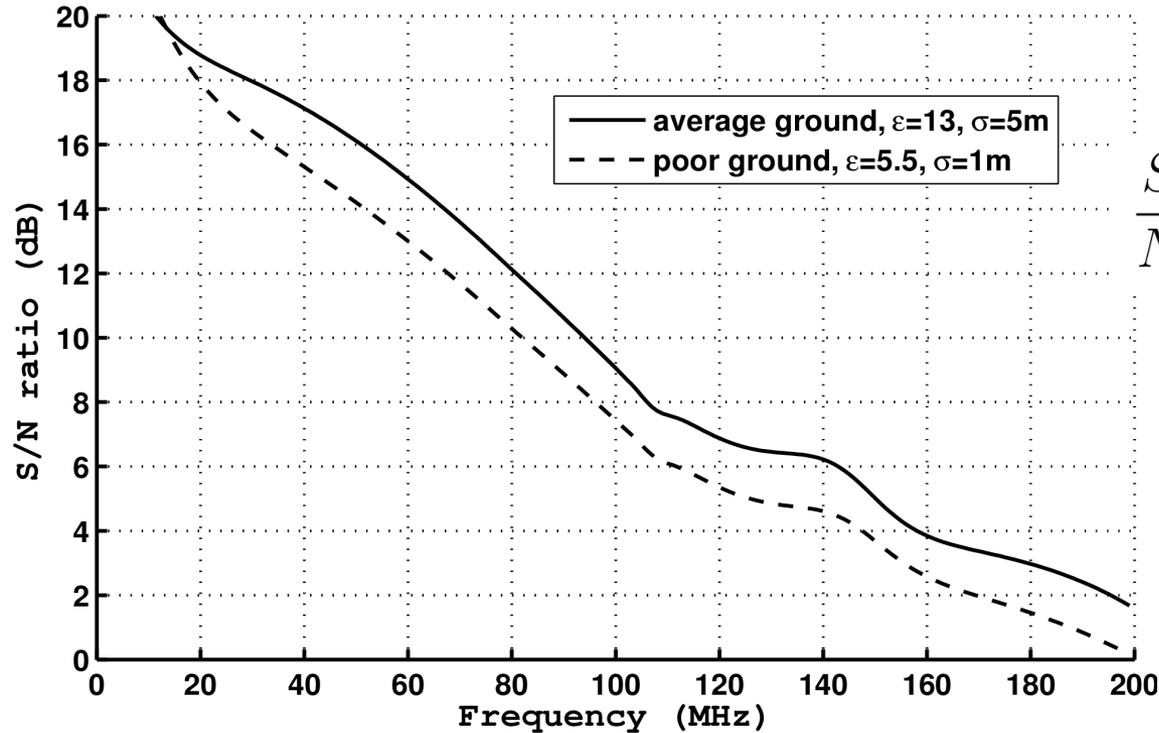
- Ultra high energy cosmic ray (UHECR)

- **For the Butterfly antenna we chose to be galactic noise dominated in [20-80]MHz even if it is not critical for UHECR radio detection**

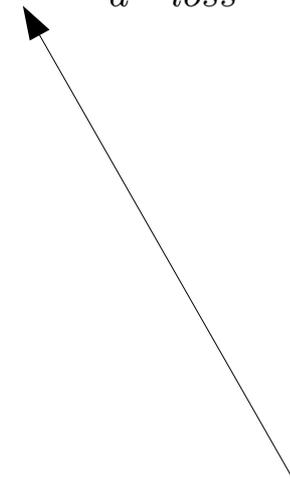
- the galactic noise can be used at least as a test source to check the antenna
- galactic noise may be used to calibrate the antenna

- **We will consider the galactic noise as a signal to qualify the Butterfly sensitivity**

# Intrinsic signal to Noise ratio of the Butterfly antenna

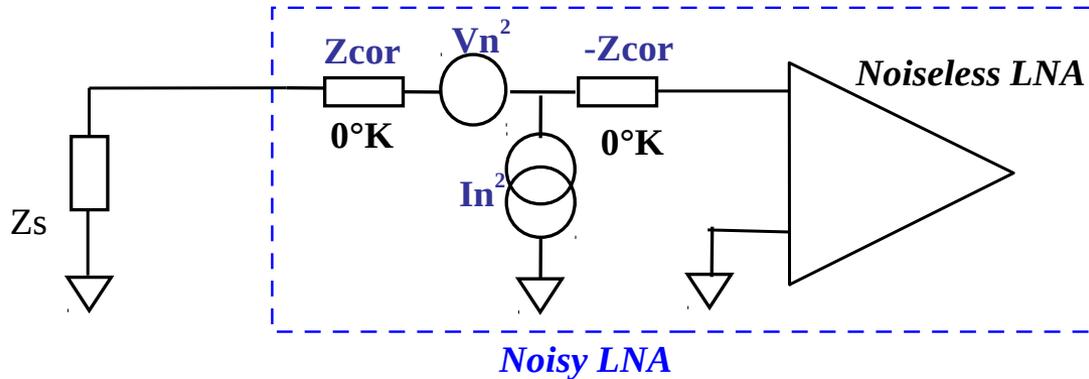


$$\frac{S_{ant}}{N_{ant}} = \frac{T_{gal} R_{rad}}{T_a R_{loss}}, \text{ with } T_a = 290K$$



- The Antenna radiator element as an intrinsic signal to noise ratio
- It limits the overall S/N (seen from the LNA output)
- It depends on the antenna geometry, the antenna height and the ground electric parameters  $\epsilon$  and  $\sigma$
- Antenna S/N is decreasing with frequency due to  $T_{gal}$  decrease and is lower than 10dB above ~100MHz ('average' ground)

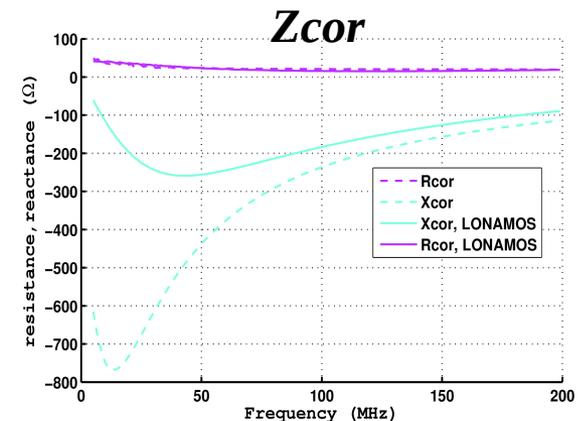
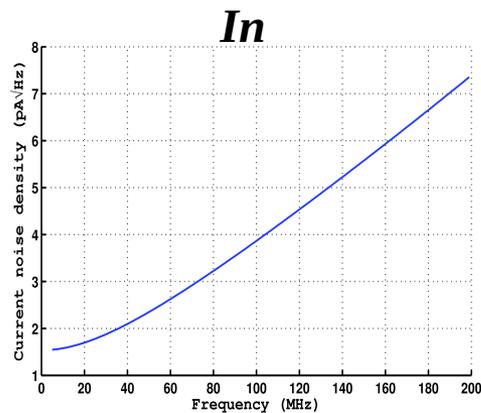
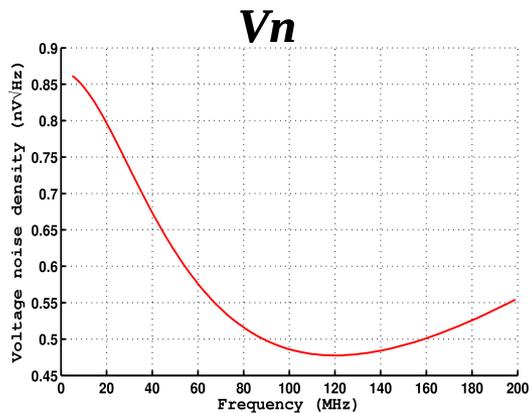
# Rothe & Dahlke noise model of the LNA



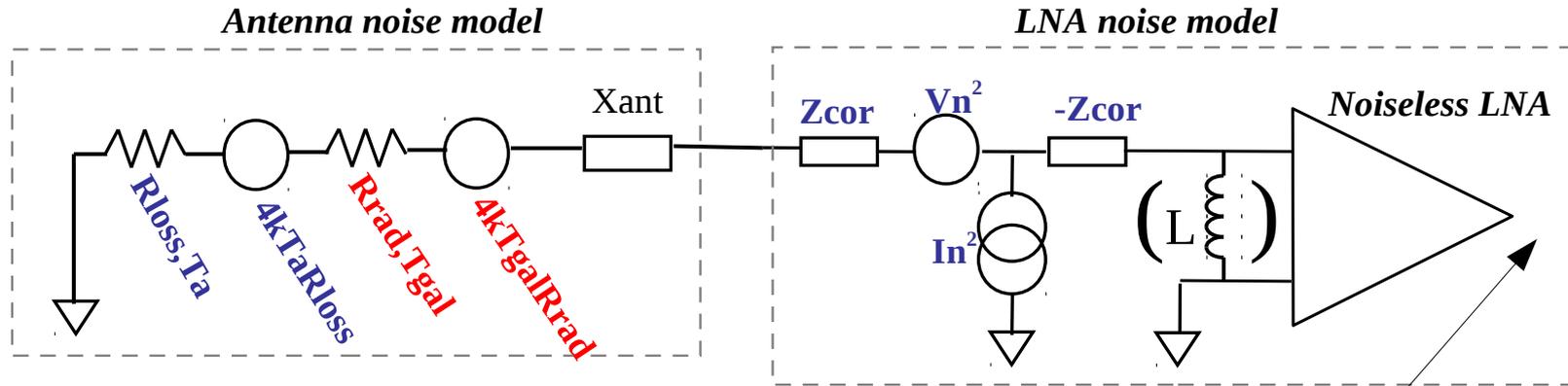
4 parameters are required to fully model the noise of a 2-port network

- $V_n$  and  $I_n$  are uncorrelated noise sources
- The correlation is model by  $Z_{cor} = R_{cor} + jX_{cor}$  at  $0^\circ\text{K}$
- the correlation impedance as no effect on the signal:  $Z_{cor} + (-Z_{cor}) = 0$  !

Parameters were extracted from simulation on the LONAMOS LNA and cross checked with measurements using reference source impedances: error < 3%



# Calculating Signal to noise ratio from the full noise model



$$\frac{S_{out}}{N_{out}} = \frac{\frac{T_{gal}}{T_a} R_{rad}}{\left(\frac{1-\eta}{\eta}\right) R_{rad} + r_n + g_n \left[ \left(\frac{R_{rad}}{\eta} + R_{cor}\right)^2 + (X_{ant} + X_{cor})^2 \right]}$$

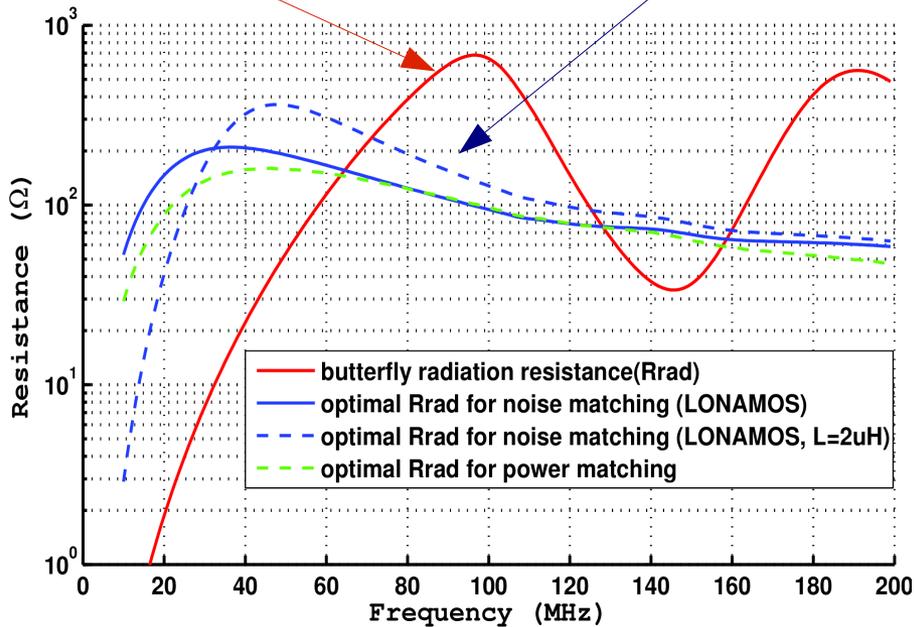
$$r_n = \frac{v_n^2}{4kT_a}$$

$$g_n = \frac{i_n^2}{4kT_a}$$

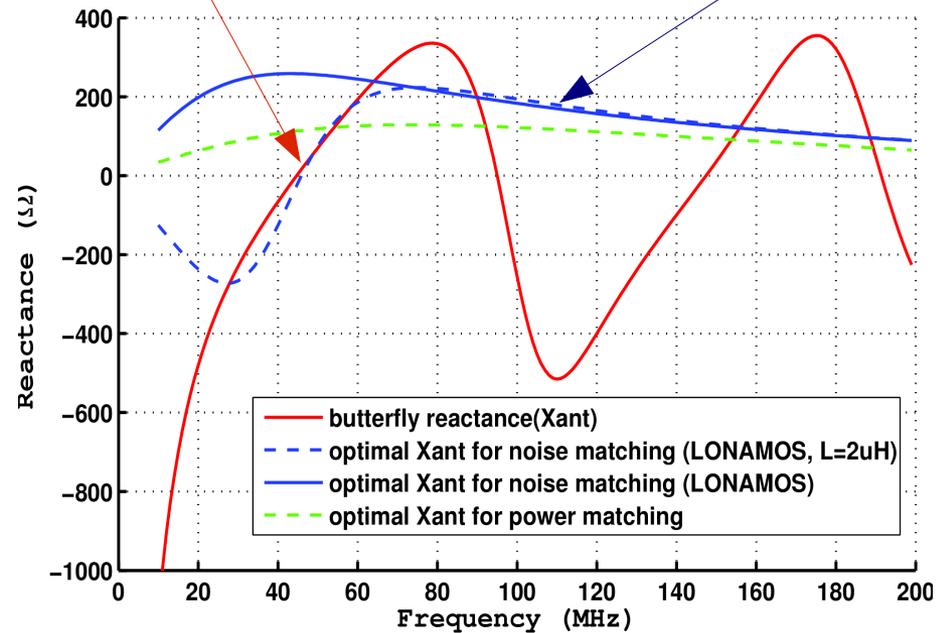
- From the full noise model, we calculate the total S/N at the LNA output
- The Butterfly antenna is active: LNA placed at the antenna feedpoint
  - ==> power matching is not required
  - ==> noise matching becomes possible
- 1st solution: adjusting the LNA parameters ( $r_n$ ,  $g_n$  and  $Z_{cor}$ )
  - minimizing  $g_n$  ...
  - cancelling  $X_{ant}$  by  $X_{cor}$

# Towards noise matching

**Butterfly Rrad and optimal LNA Rrad**



**Butterfly Xant and optimal LNA Xant**



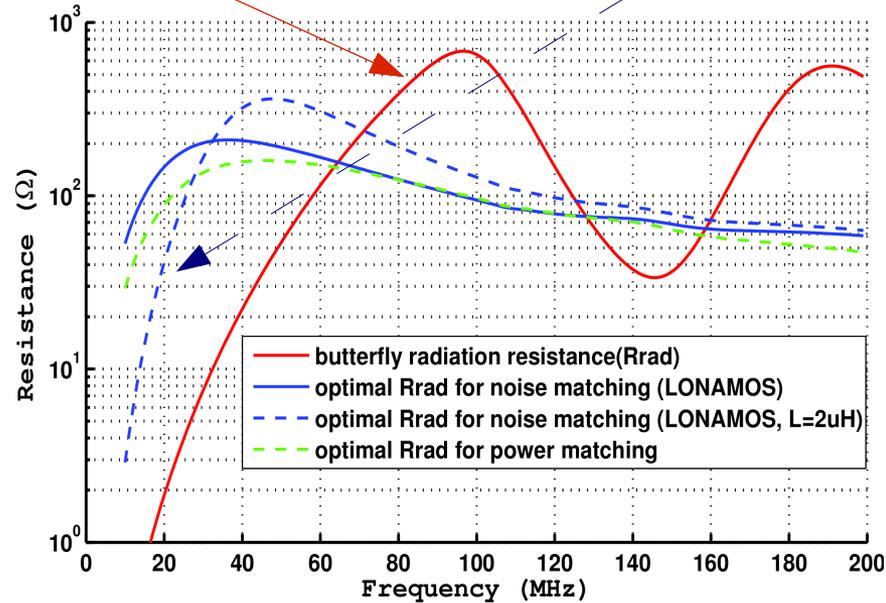
$$R_{rad}^{opt} = \eta \sqrt{R_{cor}^2 + \frac{r_n}{g_n}}$$

$$X_{ant}^{opt} = -X_{cor}$$

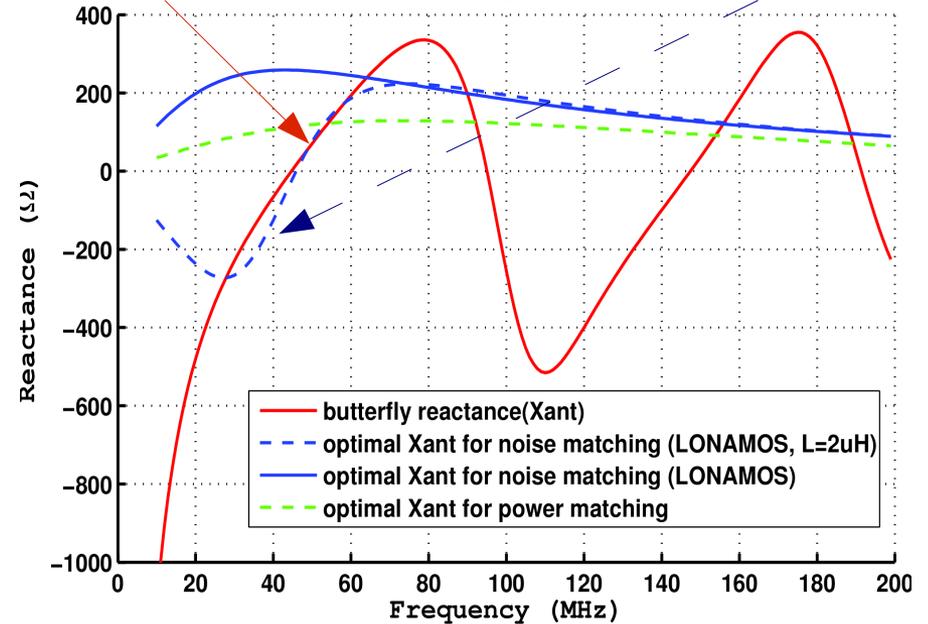
- **2nd solution: adjusting the antenna parameters (Rrad, Xant and  $\eta$ )**
  - we calculate the optimum Rrad and Xant that maximize the S/N for a given LNA configuration and a given antenna efficiency
  - We need to decrease the Antenna reactance and radiation resistance variation
  - ==> **FAT dipole**

# Towards noise matching

**Butterfly Rrad and optimal LNA Rrad with L**



**Butterfly Xant and optimal LNA Xant with L**

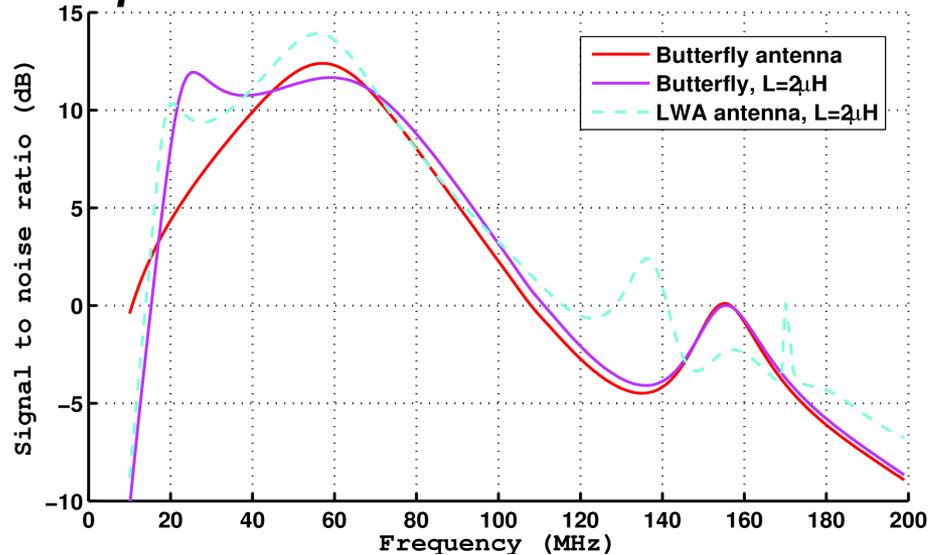


## 3rd solution: adding a noise matching array between the antenna and the LNA

- noiseless passive components (transformer, inductance, capacitance)
- The inductance L connected at the LNA input has 2 purpose
  - filtering low frequencies RFI
  - enhance the low frequencies noise matching
- ==> noise matching becomes much better in the 15-40MHz band !
- but, additional matching array may increase the group delay variation

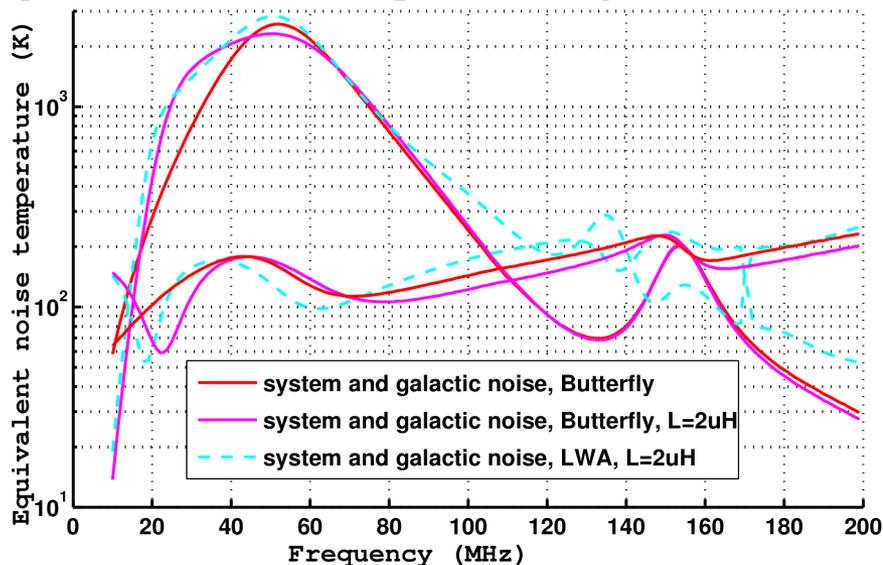
# Signal to Noise ratio of the Butterfly antenna

## S/N of the BUTTERFLY with LONAMOS LNA



- S/N of the Butterfly-LONAMOS is more than 10dB in  $\sim[40-72]\text{MHz}$
- The bandwidth is increased to  $\sim[22-75]\text{MHz}$  with a noise matching inductance

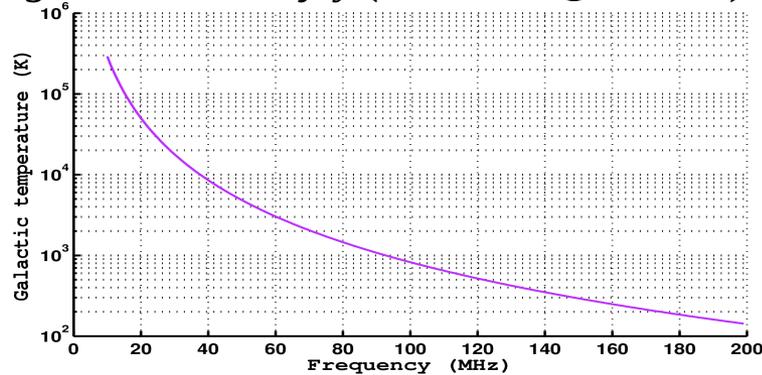
## Equivalent noise temperature of the LONAMOS-BUTTERFLY



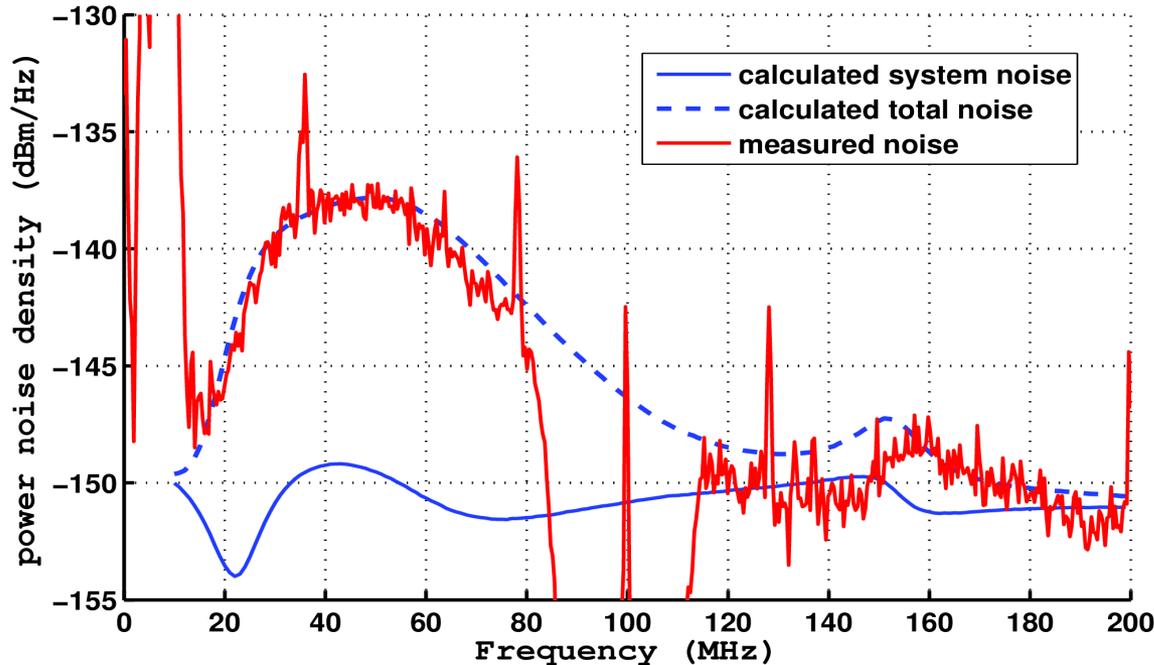
- The equivalent noise temperature of the LNA and the Butterfly losses with the Butterfly impedance as source is less than 200K

# Noise measurement versus simulation on the galaxy level

*Known galactic temperature data for the minimum galactic at Nançay ( $T=4830\text{K}$  @  $50\text{MHz}$ )*



*Measurement performed December, 17 2013 at 5H21UTC, minimum galactic*

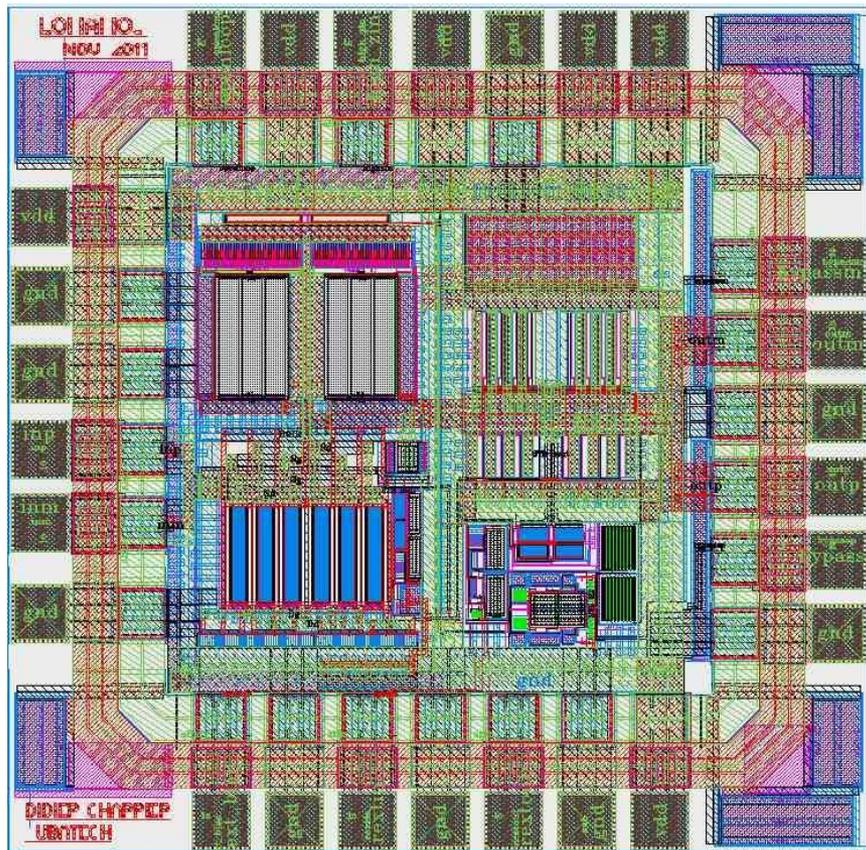


Absolute noise calculation match the measurement.

==> The noise model is fine

# The LONAMOS LNA

## *the LONAMOS layout*

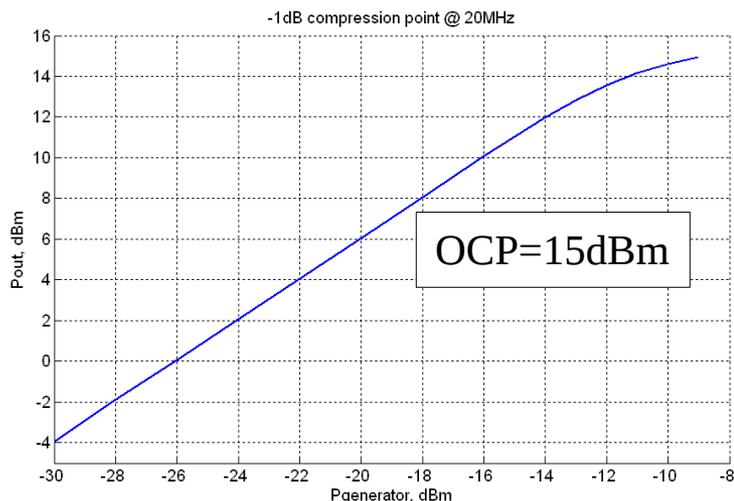


- Fully differential architecture
  - reject even order harmonic products
  - reject common noises
  - no input BALUN required
- Adjustable input impedance

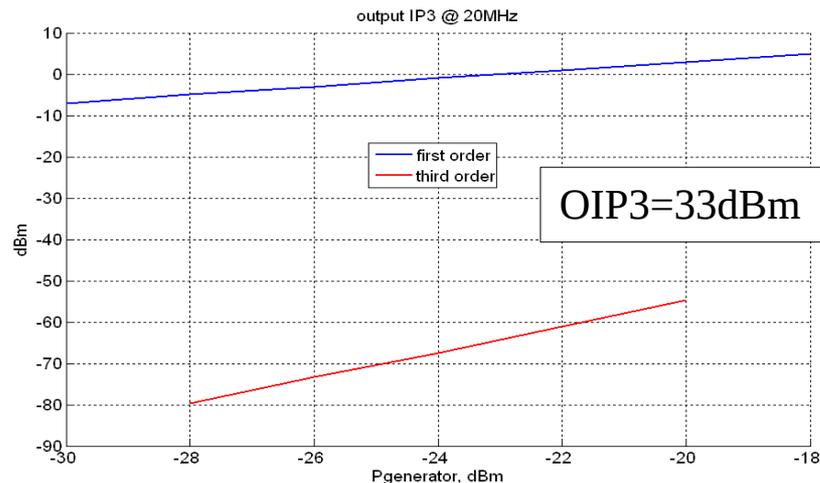
- ASIC (Application Specific Integrated Circuit) designed in 2011 to substitute to the CODALAMP with an up to date technology
- Main goal:
  - Increase the linearity characteristics
  - Decrease the temperature drift and gain uncertainty
- Use the unexpensive AMS CMOS 0.35 $\mu$  technology
- Area: 1400 $\mu$  x 1400 $\mu$

# LONAMOS measurements, OCP, OIP3, NF

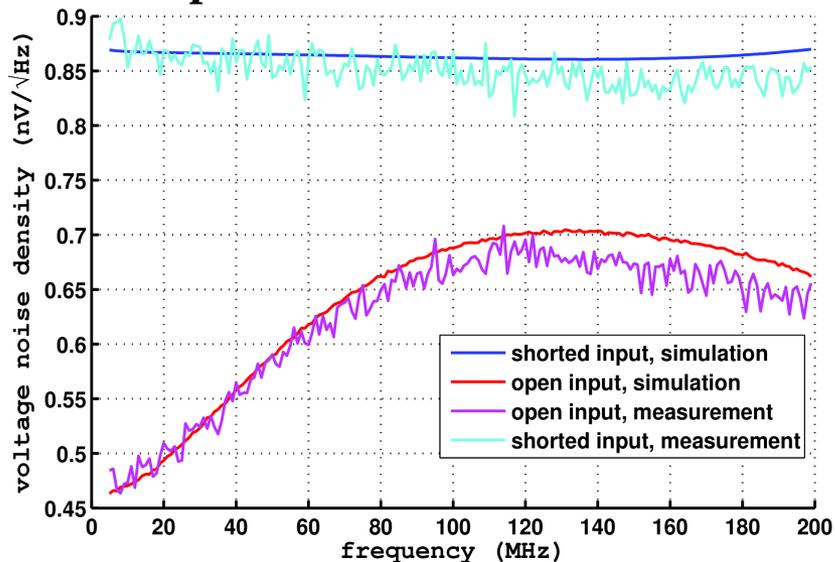
## Output compression point measurement



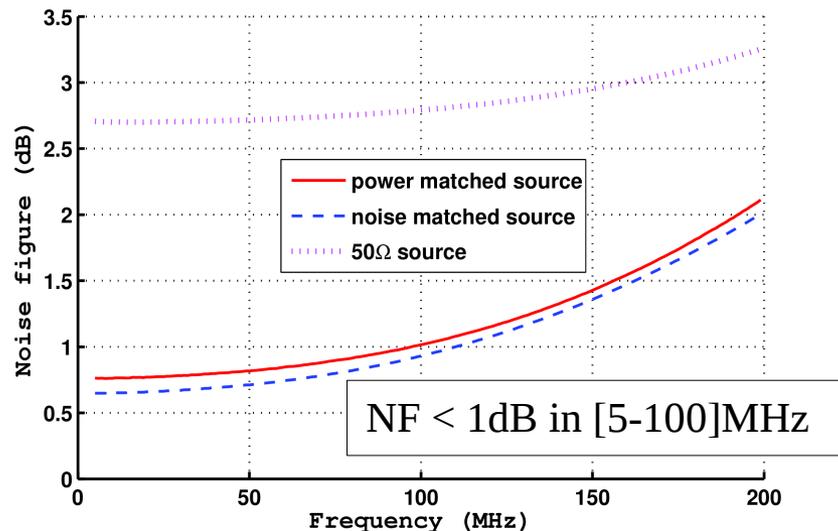
## Output 3rd order intercept point measurement



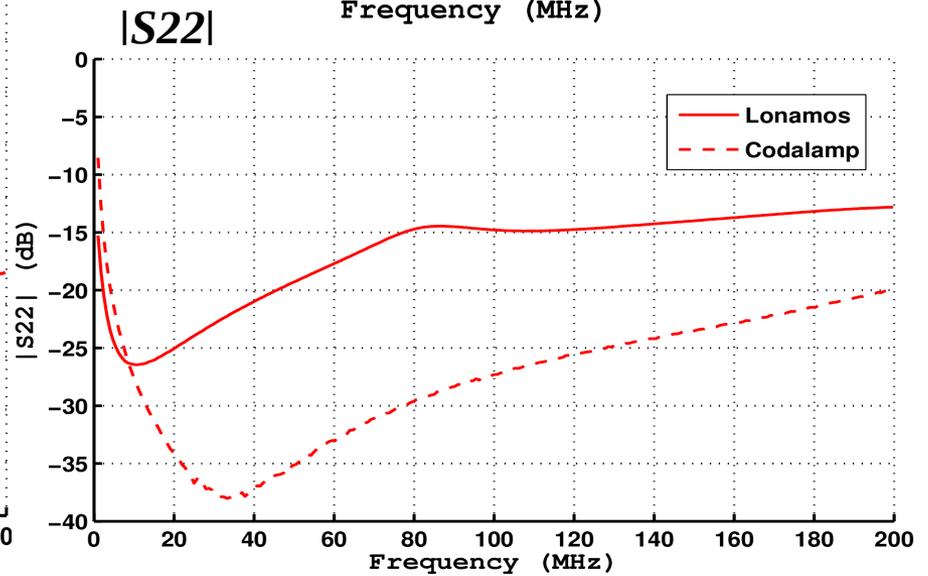
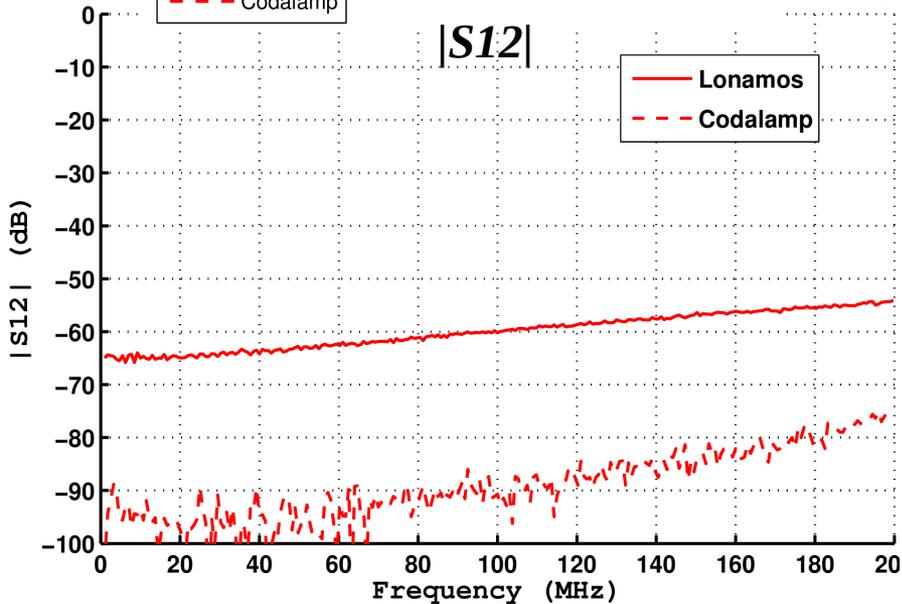
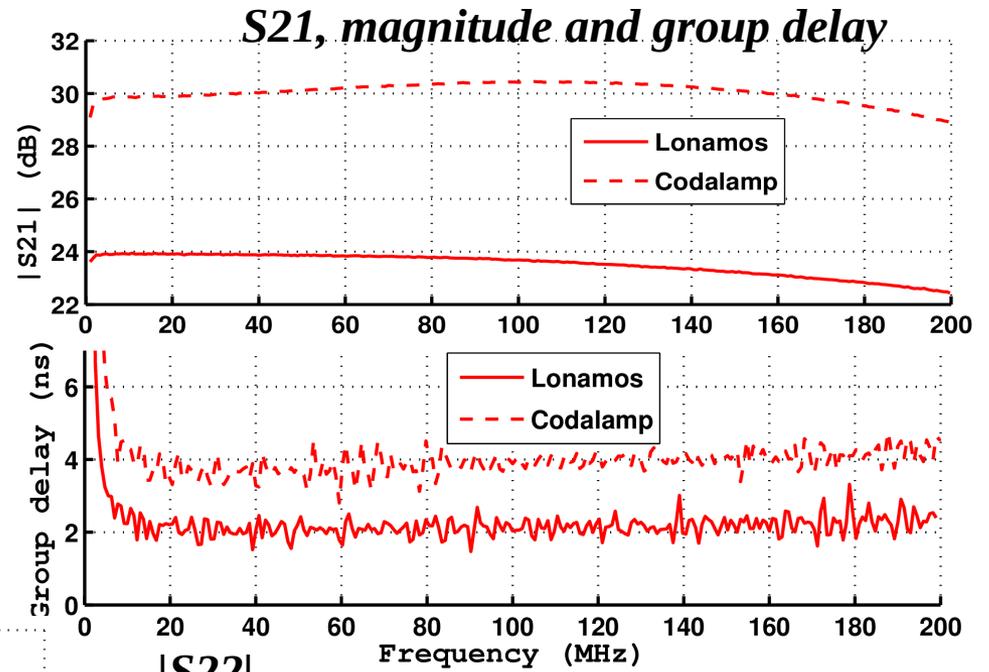
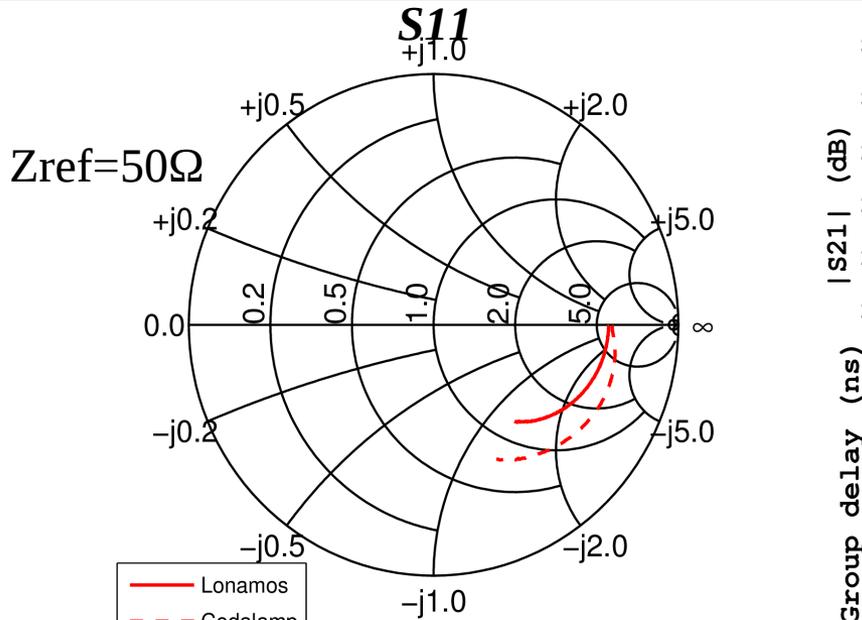
## Total output noise measurement/simulation



## Noise Figure



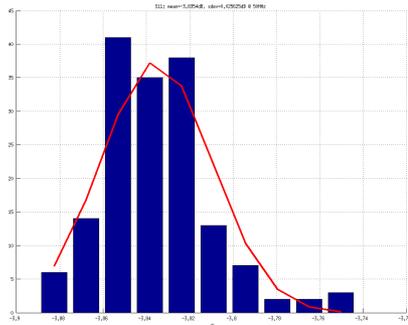
# LNA measurements, Scattering parameters



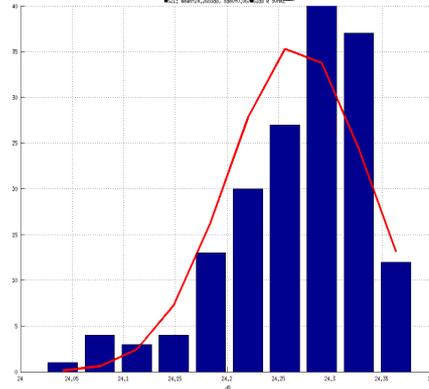
# Uncertainty measurements

LONAMOS histogram, N=160

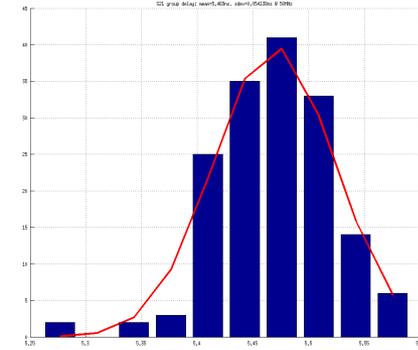
**|S11| @ 50MHz**



**|S21| @ 50MHz**

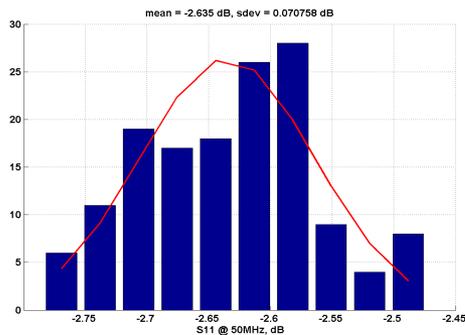


**group delay (S21) @ 50MHz**

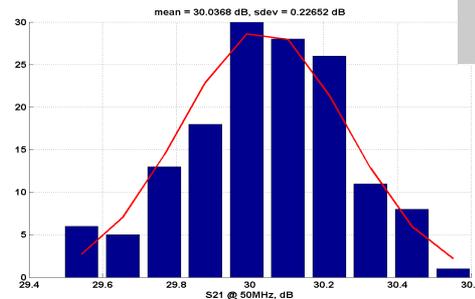


CODALAMP histogram, N=146

**|S11| @ 50MHz**



**|S21| @ 50MHz**



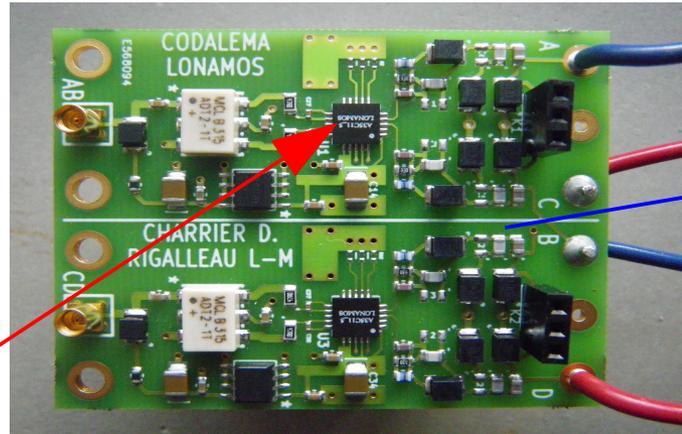
@50MHz	LONAMOS	CODALAMP
S11 , dB m dB	$\mu=-3.84$ $\sigma=26$	$\mu=-2.6$ $\sigma=71$
S21 , dB m dB	$\mu=24.27$ $\sigma=67$	$\mu=30$ $\sigma=227$
GD(S21), ns ps	$\mu=5.47$ $\sigma=54$	$\mu=$ $\sigma=$

# LNA characteristics, summary and comparison

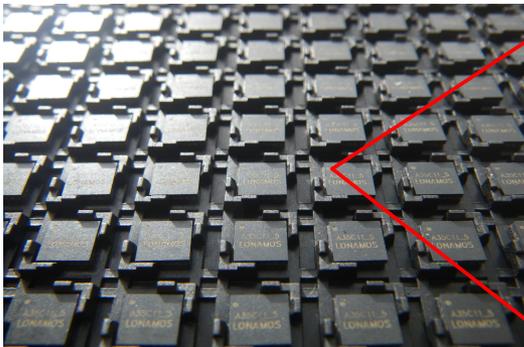
	CODALAMP	LONAMOS	
OIP3, dBm	14	33	
OCP(-1dB), dBm	0	15	* ICP is 21dB higher
Gp, dB	33	<b>27</b>	* gain is 6dB lower
IIP3, dBm	-19	6	* IIP3 is 25dB higher
IIP3, Volt	0.063	<b>1.1</b>	
NF(matched), dB		<b>0.8</b>	* NF is less than 1dB in [5-100]MHz
NFOptimal, dB		0.7	
NF (50Ω), dB	~3.5	2.7	
Band, MHz	>200	>200	
Sdev(Gain), dB	0.23	<b>0.07</b>	* Gain Dispersion is 3 times lower
Sdev(GD(Gain)),ps		50	
T° drift, mdB/°C	-26	<b>-4</b>	* Temperature drift is 6 times lower
consumption, mW	310	340	* Consumption is similar

# The LONAMOS LNA boards

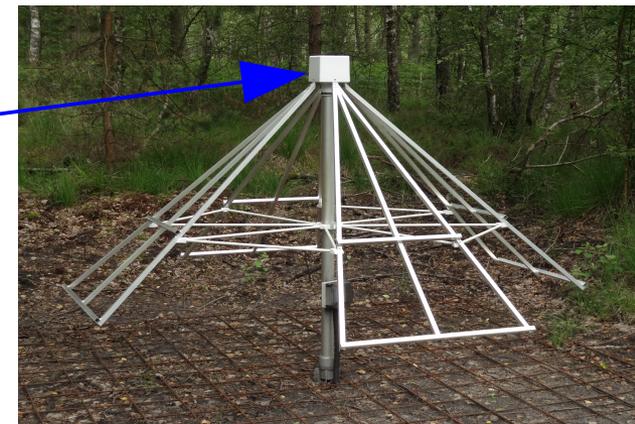
*The CODALEMA-LONAMOS LNA board: equip Butterfly antennas*



*The LONAMOS chip: ~800 circuits were produced*



*The NenuFAR-LONAMOS LNA board: equip LWA antennas*

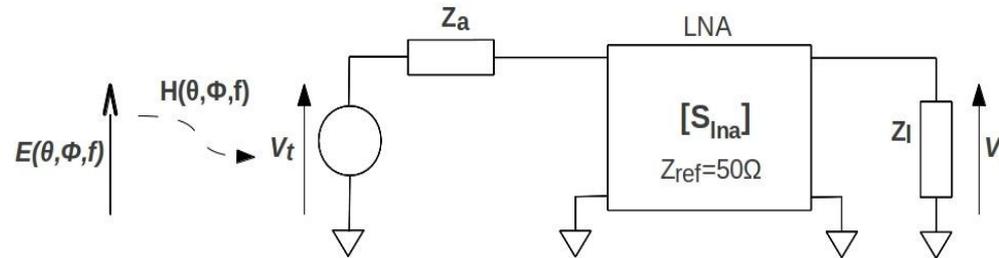


# Antenna isotropy in the time domain

- Antenna are often characterized in the frequency domain by  $|G|$ 
  - But We need the phase to work in the time domain !
- ==> we use the vector equivalent length  $H_{bfy}$  calculated as the product of
  - The antenna vector effective height...
  - ...by the transfer function from the antenna terminal point to the LNA output

$$\vec{H}_{(\theta,\phi,f)}^{bfy} = j \frac{2c}{\eta I_t f} \vec{E}_{(\theta,\phi,r,f)} r e^{\frac{j2\pi f r}{c}} \frac{S_{21}}{\frac{Z_{ant}}{Z_{ref}} (1 - S_{11}) + (1 + S_{11})}$$

with  $Z_{ref}$  the reference impedance,  $\eta=377\Omega$ ,  $I_t$  is the current value used for the transmitting mode simulation,  $E$  the vector simulated electric field simulated with NEC

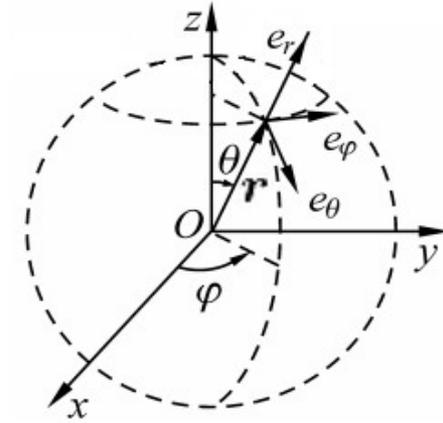
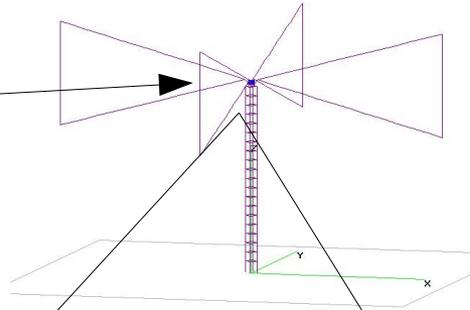
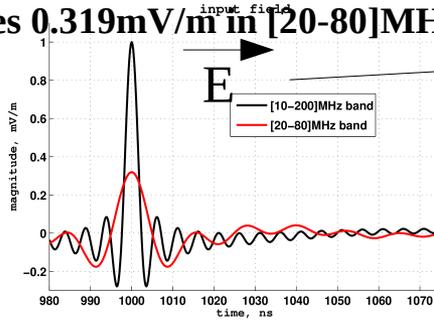


- The vector equivalent length is calculated along the theta and phi direction of a spherical coordinate system
- The vector equivalent length knowledge is necessary to unfold the antenna response and calculate the received electric field in time or frequency domain

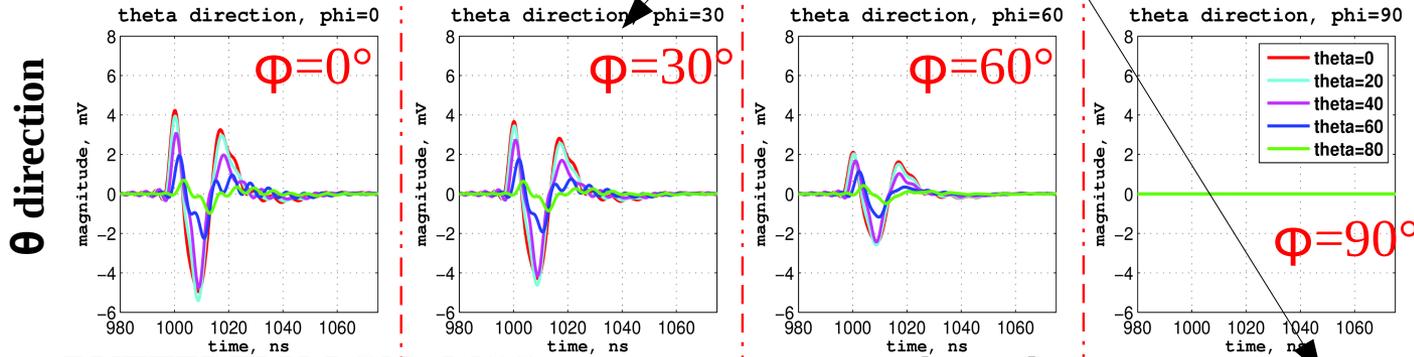
# Butterfly response to a Dirac pulse

input dirac bandwidth limited to [10-200]MHz  
and normalized to 1mV/m

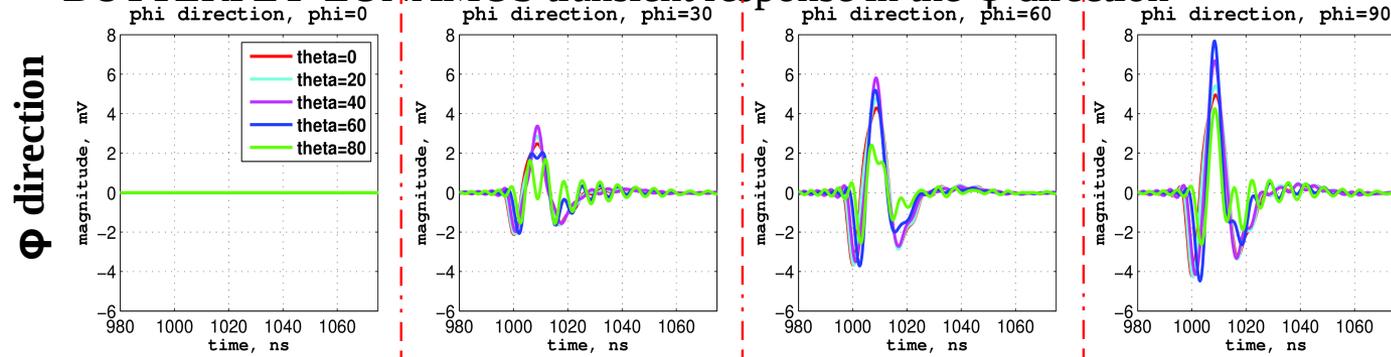
==> gives 0.319mV/m in [20-80]MHz



BUTTERFLY-LONAMOS transient response in the  $\theta$  direction

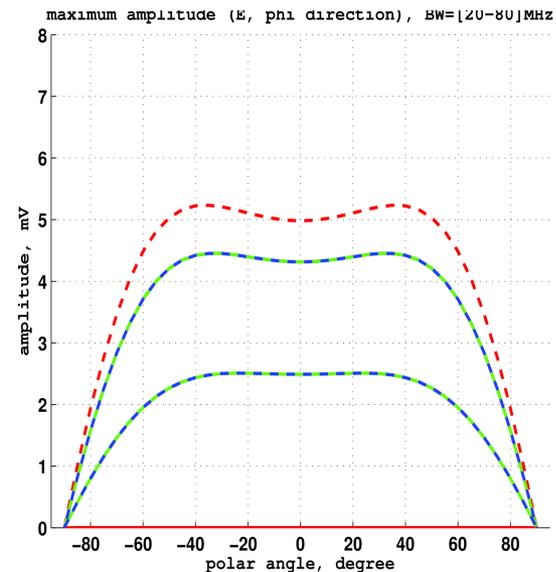
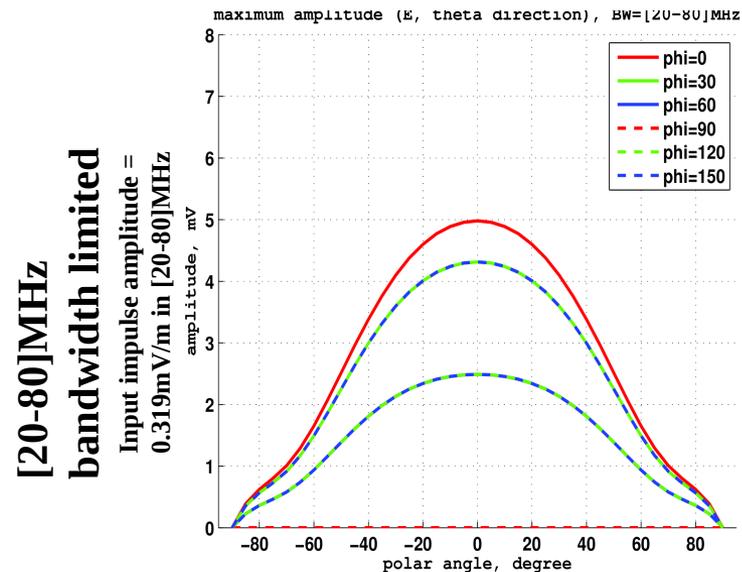
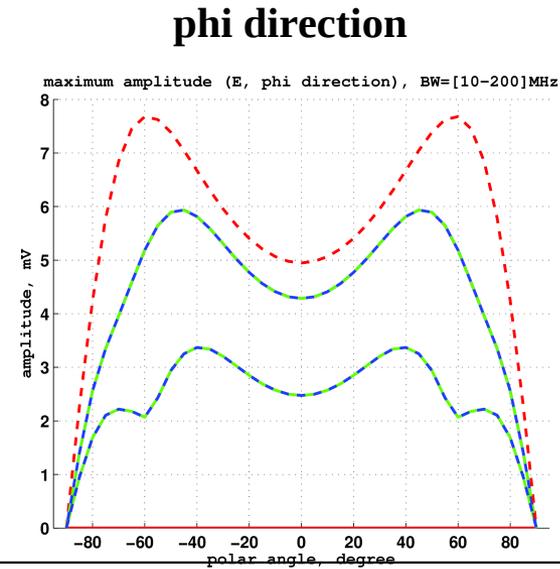
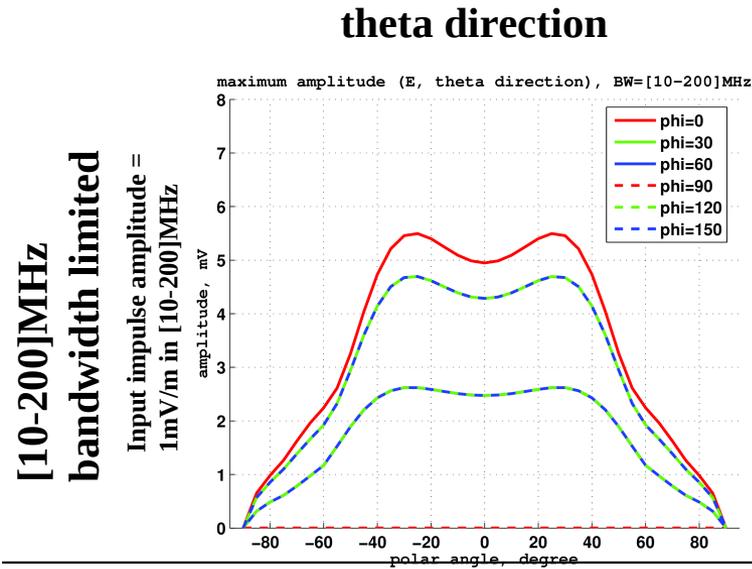


BUTTERFLY-LONAMOS transient response in the  $\phi$  direction



# Time domain 'isotropy pattern'

We calculate a time domain pattern  $\max(|V|(t))$  as a function of  $\theta$ ,  $\varphi$  and the bandwidth



- **The Butterfly antenna is used by many experiments**
  - CODALEMA, Nançay, France: 60 antennas
  - AERA, Malargüe, Argentina: 100 antennas
  - HELYCON, Greece: 6 antennas
  - TREND, Ulaštai, China: 54 antennas
- **The LONAMOS LNA improves characteristics**
  - Linearity
  - Gain uncertainty
  - Temperature drift
  - Sensitivity
- **The LONAMOS gives good results with the LWA antenna on**
  - COMPACT ARRAY, Nançay, France: 10 antennas
  - NenuFAR, Nançay, France: ~57 antennas (~2000 antennas foreseen)
- **A three polarization 'Butterfly like' antenna is under study**

Thank you for your  
attention